Complete Wetting in the Three-Dimensional Transverse Ising Model

A. B. Harris, ¹ C. Micheletti, ² and J. M. Yeomans²

Received November 3, 1995

We consider a three-dimensional Ising model in a transverse magnetic field h and a bulk field H. An interface is introduced by an appropriate choice of boundary conditions. At the point $(H=0,\ h=0)$ spin configurations corresponding to different positions of the interface are degenerate. By studying the phase diagram near this multiphase point using quantum mechanical perturbation theory, we show that the quantum fluctuations, controlled by h, split the multiphase degeneracy giving rise to an infinite sequence of layering transitions.

KEY WORDS: Ising models; ground-state selection; layering transition; wetting.

1. INTRODUCTION

There is a considerable body of literature discussing the way in which interfaces depin from surfaces.⁽¹⁾ Of particular interest to us here is the situation below the roughening transition when the interface is smooth and can depin from the surface through a series of first-order layering transitions.

This possibility was first pointed out by De Oliveira and Griffiths⁽²⁾ for a model in which the layering is driven by the competition between a long-range bulk interaction and a surface field. Here the layering transitions exist even at zero temperature. Later Duxbury and Yeomans⁽³⁾ showed that, if the position of the interface relative to the surface was degenerate at zero temperature, the degeneracy could be split by thermal fluctuations giving an infinite series of layering transitions at finite temperatures. The stable interface position is determined as a balance between

¹ Department of Physics, University of Pennsylvania, Philadelphia, Pennsylvania 19104-6396.

² Theoretical Physics, Oxford University, Oxford OX1 3NP, U.K.

the binding effect of a bulk field and the entropic advantage for the interface lying further from the surface.

The transverse Ising model⁽⁴⁾ was first introduced by de Gennes⁽⁵⁾ in connection with ferroelectric materials. Recently Henkel *et al.*⁽⁶⁾ have discussed the behavior of a domain wall in this system. The interesting questions concern the effect of *quantum* fluctuations, mediated by the transverse field, on the behavior of the interface. Their work considers one dimension where the interface is rough. Very different behavior is likely for a smooth interface. Therefore in this paper we consider the behavior of the three-dimensional transverse Ising model below the roughening temperature. We find that a zero-temperature multiphase point can be split by quantum fluctuations and that, for a nonzero transverse field, there is an infinite number of stable positions for the interface as a longitudinal bulk field passes through zero.

The next section defines the model and gives a qualitative discussion of its properties and our approach. Quantitative details of the calculation, which is based on quantum mechanical perturbation theory, are given in Section 3. Our conclusions are summarized in Section 4.

2. QUALITATIVE REMARKS

The Hamiltonian of the three-dimensional transverse Ising model we shall consider is

$$\mathcal{H} = -J_{0} \sum_{i=1,L} \sum_{\langle j,j' \rangle} S_{z}(i,j) S_{z}(i,j') - J_{1} \sum_{i=0,L} \sum_{j} S_{z}(i,j) S_{z}(i+1,j)$$

$$-\sum_{i=1,L} \sum_{j} [hS_{x}(i,j) + HS_{z}(i,j)]$$

$$-K \sum_{j} (S_{z}(0,j) - S_{z}(L+1,j))$$
(2.1)

where i labels two-dimensional planes and $\langle j,j'\rangle$ pairs of nearest neighbors within a plane. The parameter $K\to\infty$ is used to impose appropriate boundary conditions, namely to fix the spins at the surface (i=0) to be up and those in the last layer (i=L+1) to be down. These boundary conditions will create a domain wall, or interface, in the system separating layers of up and down spins (see Fig. 1). Our aim is to construct the phase diagram which gives the position k of the interface (defined as in Fig. 2a) as a function of the longitudinal bulk field K and the transverse field K we shall consider the limit $K\to\infty$ and zero temperature, where the interface is flat.

As a first step in understanding the phase diagram we consider the situation for h = 0. In this case it is clear that for positive H, $k = \infty$,

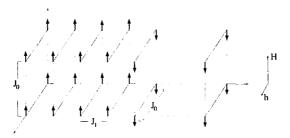


Fig. 1. Schematic representation of the model introduced in Eq. (2.1). The leftmost plane is labeled i = 0 and the rightmost i = L + 1. The surface field K is not shown.

whereas for negative H, k=0. We shall call these phases, which are illustrated in Fig. 2, R and L, respectively. For H=0 the energy is independent of k, so that all interface positions are degenerate. It is known that such a degeneracy can be lifted by either thermal fluctuations⁽⁷⁾ or quantum fluctuations.⁽⁸⁾ In more general contexts this removal of degeneracy has been referred to as ground-state selection,⁽⁹⁾ following the work of Villain and Gordon⁽¹¹⁾ and Shender.⁽¹⁰⁾ Here we will consider the effect of quantum fluctuations.

There are two possibilities: in the first, quantum fluctuations due to nonzero h cause the transition from L to R to be discontinuous with no intermediate states; in the second this transition occurs through a sequence of intermediate states in which k increases monotonically. This sequence can be finite, so that there is a first-order transition from a state with $k = k_{\text{max}}$ to R, or it can be infinite. In general, one expects the first possibility when the effective interaction between the surface and the interface is attractive and the second when this effective interaction is repulsive.

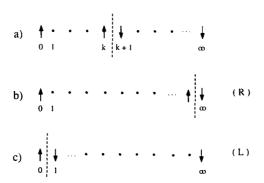


Fig. 2. (a) Configuration of the spins when the interface is at position k. Layer 0 is constrained to be up and the layer at infinity is constrained to be down. (b) Configuration R; (c) configuration L.

Our results indicate that quantum effects give rise to the second possibility and that the sequence of layering transitions is probably an infinite one. It is easy to see that even when h is nonzero, the R phase is stable whenever H is positive. As we will show, the stability of the L phase requires that $H < -Ch^2J_1/J_0^2$, where C is a constant.

To determine the interface position we must calculate the ground-state energy as a function of H. To do this we assume perfectly flat interfaces and apply perturbation theory in h to calculate the energy of the state when the interface is at position k. If we were dealing with a finite system, perturbation theory would introduce coupling in finite order between states when the interface is at different positions. However, this tunneling effect disappears in the thermodynamic limit. Our calculations are valid for $h \ll J$. We also impose the condition $J_1 \ll J_0$, although as long as we remain in the regime where the interfaces are flat, this restriction is probably inessential.

The energy per layer spin e(k) of the state when the interface is at position k can be written

$$e(k) = e_0(H) - kH + E_k(H)$$
 (2.2)

where $e_0(H)$ is the energy per layer spin for the k=0 phase. The most important dependence on H is in the term -kH. In addition, H also contributes to the energy denominators that appear in perturbation theory, which are typically of the form $2J_0+J_1+H$. However, perturbative contributions to $E_k(H)$, when expanded in powers of H, lead to corrections which are of relative order H/J_0 or smaller. But since we will only be interested in H in the range $-Ch^2/J_0 < H < 0$, these corrections are smaller than of relative order $(h^2/J_0^2) \le 1$, which we may ignore. Therefore, in Eq. (2.2), we may evaluate $E_k(H)$ at H=0. We shall find that E_k is a positive and decreasing function of k. This result leads to an infinite sequence of phase transitions. The critical field separating the phase k from k+1 is given by

$$-H_k^* = E_k - E_{k+1} \equiv \Delta E_k \tag{2.3}$$

where, as argued above, the leading-order calculation of E_k can be obtained for H = 0.

3. CALCULATION OF ΔE_{κ}

From Eq. (2.3) it is clear that we only need to keep track of terms in the ground-state energy which depend on k. In other words we need to ascertain how the corrections to the ground-state energy which are perturbative in k depend on the location of the interface. For convenience we

now transform to occupation number operators. For spins that are up [down] we write $S_z(i, j) = 1/2 - n_{i,j} [S_z(i, j) = -1/2 + n_{i,j}]$. Also $S_x(i, j) = (a_{i,j}^{\dagger} + a_{i,j})/2$, where the operator $a_{i,j}^{\dagger}(a_{i,j})$ creates (destroys) a Bose excitation at site i in the jth layer and $n_{i,j} = a_{i,j}^{\dagger} a_{i,j}$. Strictly speaking, we should not allow more than one excitation to exist on a single site. To enforce this restriction we include a term of the form $A \sum_{i,j} a_{i,j}^{\dagger} a_{i,j}^{\dagger} a_{i,j} a_{i,j}$, where $A \to \infty$. Normally, it is difficult to take full account of such a hard-core interaction. As we will see, we accommodate this constraint by never involving matrix elements connecting to a state in which there is more than one excitation at any site. Therefore, setting H = 0, we are led to the following bosonic Hamiltonian, when the interface is at position k:

$$\mathcal{H}_{B} = E_{0} + \sum_{i=1}^{\infty} \sum_{j} (2J_{0}n_{i,j} - (h/2)[a_{i,j}^{\dagger} + a_{i,j}])$$

$$- \sum_{i=1}^{\infty} \sum_{\langle j,j' \rangle} J_{0}n_{i,j}n_{i,j'} + \Lambda \sum_{i=1}^{\infty} \sum_{j} a_{i,j}^{\dagger} a_{i,j}^{\dagger} a_{i,j} a_{i,j}$$

$$- J_{1} \sum_{i=0}^{\infty} \sum_{j} [-(1/2)(n_{i,j} + n_{i+1,j}) + n_{i,j}n_{i+1,j}]$$

$$+ J_{1} \sum_{j} [-n_{k,j} - n_{k+1,j} + 2n_{k,j}n_{k+1,j}]$$
(3.1)

where E_0 is the unperturbed energy of the k=0 phase, $\Lambda \to \infty$, and for $K \to \infty$, we may set $n_{0,j} = 0$. We write this Hamiltonian as

$$\mathcal{H}_B = E_0 + \mathcal{H}_0 + V_1 + V_2 + V_3 + V_4 \tag{3.2}$$

where

$$\mathcal{H}_0 = \Delta \sum_{i} \sum_{j} n_{i,j} \tag{3.3}$$

with $\Delta = 2J_0 + J_1$,

$$V_1 = -\sum_{i} \sum_{j} J_{i,i+1} n_{i,j} n_{i+1,j} - J_0 \sum_{j} \sum_{\langle i,j' \rangle} n_{i,j} n_{i,j'}$$
 (3.4)

$$V_2 = -(h/2) \sum_{i} \sum_{j} \left[a_{i,j}^{\dagger} + a_{i,j} \right]$$
 (3.5)

$$V_3 = -J_1 \sum_j (n_{k,j} + n_{k+1,j})$$
(3.6)

where

$$J_{i,i+1} = \begin{cases} J_1 & \text{for } i \neq k \\ -J_1 & \text{for } i = k \end{cases}$$
 (3.7)

and (with $\Lambda \to \infty$)

$$V_4 = \Lambda \sum_i \sum_j a_{i,j}^{\dagger} a_{i,j}^{\dagger} a_{i,j} a_{i,j}$$
(3.8)

We now consider how the perturbative contributions to the energy depend on the various coupling constants. To carry out this discussion it is convenient to introduce a diagrammatic representation of the contributions to the perturbation expansion. Each term of V_1 proportional to $J_{rs}n_rn_s$, where r (and similarly s) denotes a position label of the form i, j, is represented by a line joining the two interacting sites r and s and s and s and s are in the same plane or are in adjacent planes. The perturbation in s0 proportional to s0 s1 is represented by a minus (plus) sign at the site s1. However, for simplicity, since each site involved with any of the other interactions must be excited (i.e., must have both s2 and s3. The term in the perturbation s3 proportional to s4 s5 in Fig. 3. The term in the perturbation s4 proportional to s5 s6 s7 is represented by a circle attached to the site s7 s8 proportional to s8 s9 proportional to s9 proportion

We now define what we mean by connected terms. Any term which involves only a single site is connected. Terms which involve more than one site are connected only if all such sites are connected with respect to lines representing terms of V_1 . If this is not the case, the term will be called disconnected. Thus diagrams (a) and (d) of Fig. 3 are disconnected.

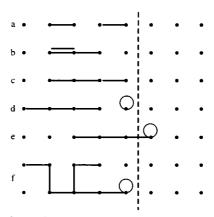


Fig. 3. Representation of perturbative contributions to the ground-state energy. The dashed line corresponds to the location of the interface. Contributions which involve J_1 and h for four sites (a) and (c) and for three sites (b) with one of the J_1 's taken to second order. (d-f) Terms which involve factors of V_3 . Diagram (f) represents a term which involves the J_0 interaction. Diagrams (a) and (d) are disconnected and therefore give zero contribution to the ground state energy, as discussed in the text.

We now establish that contributions from disconnected configurations of lines vanish. Consider a disconnected diagram Γ which consists of two disjoint components Γ_A and Γ_B . The contribution of this diagram is unchanged if we treat perturbatively the system $S(\Gamma_A + \Gamma_B)$ in which all coupling constants J_{rs} not in Γ_A or Γ_B are set to zero. But because Γ_A and Γ_B are disjoint systems, we have $E(\Gamma_A + \Gamma_B) = E(\Gamma_A) + E(\Gamma_B)$. This result indicates that there are no disconnected terms in the ground-state energy which involve simultaneously an exchange constant from one component Γ_A and an exchange constant from the other component Γ_B . Thus, disconnected diagrams can be omitted from further consideration.

To evaluate $\Delta E_{\rm b}$, it is apparent from the form of Eq. (2.2) that we only need to keep contributions which appear when the interface is at position k+1, but not when it is at position k. To identify the contributions which are lowest order in (J_1/Δ) and in (h/Δ) , it is convenient to refer to Figs. 4 and 5, where typical contributions to the ground state energy are shown. In particular consider contributions to ΔE_1 , some of which are shown in Fig. 5. Note that we did not include diagrams like those of Fig. 4 which involve no lines representing V_1 and one circle representing V_3 , because such diagrams occur equally for E_1 and E_2 . Similarly, one can see from the system of five layers shown in Fig. 5, that contributions which are first order in V_1 and zeroth order in V_2 occur identically in E_1 and E_2 . For both E_1 and E_2 there is one way to take V_1 spanning the wall, and three ways to take a V_1 which does not span the wall. Next in order of smallness, we consider contributions which involve one J_1 line (i.e. one power of V_1) and one circle (i.e. one power of V_3). In this case for E_2 one has the extra term labeled E2 in Fig. 5. The rule is thus: the leading contribution in (J_1/Δ) to ΔE_k arises from the contribution to E_{k+1} coming from a diagram which involves k lines (each carrying a factor J_1) which connect the surface to the interface and one circle representing V_3 .

Furthermore, we now show that it only minimal length chains which give the dominant contribution to ΔE_k . As we shall see, taking addition factors of V_1 involving J_0 leads to contributions which are higher order in (h/Δ) than those from diagrams involving only J_1 . To see this we give

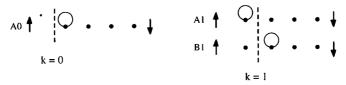


Fig. 4. Perturbative contributions to the ground-state energy used to evaluate $\Delta E_0 = E_0 - E_1$. (A0) The case when the interface is at k = 0; (A1, B1) the case k = 1.

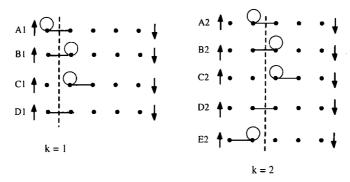


Fig. 5. Perturbative contributions to the ground-state energy used to evaluate $\Delta E_1 = E_1 - E_2$. (A1-D1) The case when the interface is at k = 1. (A2-E2) The case k = 2. The dashed line represents the position of the interface. Contributions from diagrams A1, B1, C1, and D1 are equal to those from diagrams A2, B2, C2, and D2, respectively. So ΔE_1 is determined by E2.

a more detailed analysis of the contribution of a diagram involving, say, p different lines representing V_1 and, as we explained, necessarily involving at least one interface potential term V_3 . Note that both these perturbations V_1 and V_3 involve occupation numbers n_r which vanish when there is no excitation at site r. For every site r involved in a V_1 or V_3 interaction, it is necessary to create an excitation so that n_r can be evaluated in a virtual state in which $n_r = 1$. Subsequently, in order to get back into the ground state we must destroy the excitation on the site r. Thus, in all, a diagram involving p different lines will involve p+1 sites and therefore give rise to a perturbative contribution to the energy which is of order $\delta_n E$, where

$$\delta_p E = h^{(2p+2)} J_1^{p_1} J_0^{p_2} (J_1/\Delta) / \Delta^{2p+1+p_1+p_2}$$
(3.9)

where of the p lines, p_1 are associated with J_1 and p_2 with J_0 [see Eq. (3.4)]. In writing this equation we included the factor (J_1/Δ) to take account of the necessary factor of V_3 . At this point, it is clear that to have a diagram which occurs for position k+1 but not for k it is best to invoke a linear diagram, and not one which reaches more than one row perpendicular to the interface. Unnecessary factors of J_0 in V_1 will give rise to additional factor of $J_0h^2/\Delta^3 \ll 1$. So, we conclude that no leading order

$$\Delta E_k = C_k J_0^2 [J_1 h_0^2 / J_0^3]^{k+1}$$
(3.10)

where C_k is a constant which must be determined by an explicit calculation and to leading order we set $\Delta = 2J_0$.

Now let us carry out a detailed calculation for the simplest case, namely for k = 0. From Fig. 4 we obtain

$$\Delta E_0 = -E(A1) \tag{3.11}$$

where E(A1) is the contribution to the energy in diagram A1 of Fig. 4. Thus⁽¹²⁾

$$\Delta E_{0} = -\langle 0 | V_{2} \frac{1}{\mathscr{E}} V_{3} \frac{1}{\mathscr{E}} V_{2} | 0 \rangle$$

$$= -\langle 0 | \left(\frac{-h}{2} \right) a_{1} \frac{1}{\mathscr{E}} (-J_{1} a_{1}^{\dagger} a_{1}) \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1}^{\dagger} | 0 \rangle$$

$$= \frac{h^{2}}{4} \frac{J_{1}}{\varDelta^{2}} = \frac{J_{1} h^{2}}{16J_{0}^{2}} \tag{3.12}$$

Here and below the excitation energy \mathscr{E} will be $-r\Delta = -2rJ_0$, where r is the number of excitations in the virtual state.

Next we calculate $\Delta E_1 = -E(E2)$ from diagram E2 of Fig. 5. Here we have to sum over the different orderings of the perturbations:

$$\Delta E_{1} = -\langle 0| \left[\left(\frac{-h}{2} \right) a_{1} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{2} + \left(\frac{-h}{2} \right) a_{2} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1} \right]
\times \frac{1}{\mathscr{E}} \left[\left(-J_{1} n_{1} n_{2} \right) \frac{1}{\mathscr{E}} \left(-J_{1} n_{2} \right) + \left(-J_{1} n_{2} \right) \frac{1}{\mathscr{E}} \left(-J_{1} n_{1} n_{2} \right) \right]
\times \frac{1}{\mathscr{E}} \left[\left(\frac{-h}{2} \right) a_{1}^{\dagger} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{2}^{\dagger} + \left(\frac{-h}{2} \right) a_{2}^{\dagger} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1}^{\dagger} \right] |0\rangle
- \langle 0| \left[\left(\frac{-h}{2} \right) a_{1} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{2} + \left(\frac{-h}{2} \right) a_{2} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1} \right]
\times \frac{1}{\mathscr{E}} \left(-J_{1} n_{1} n_{2} \right) \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1}^{\dagger} \frac{1}{\mathscr{E}} \left(-J_{1} n_{2} \right) \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{2}^{\dagger} |0\rangle
- \langle 0| \left(\frac{-h}{2} \right) a_{1}^{\dagger} \frac{1}{\mathscr{E}} \left(-J_{1} n_{2} \right) \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1} \frac{1}{\mathscr{E}} \left(-J_{1} n_{1} n_{2} \right)
\times \frac{1}{\mathscr{E}} \left[\left(\frac{-h}{2} \right) a_{1}^{\dagger} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{2}^{\dagger} + \left(\frac{-h}{2} \right) a_{2}^{\dagger} \frac{1}{\mathscr{E}} \left(\frac{-h}{2} \right) a_{1}^{\dagger} \right] |0\rangle$$
(3.13)

When simplified this yields

$$\Delta E_1 = 2(h/2)^4 J_1^2 / \Delta^5 = (1/256) J_1^2 h^4 / J_0^5$$
 (3.14)

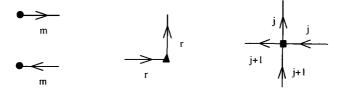


Fig. 6. Vertices for Matsubara diagrams. (a) Transverse field vertex $-(h/2)(a_m^{\dagger})$ (top) and $-(h/2) a_m$ (bottom); (b) $-J_1 \delta_{r,k} a_r^{\dagger} a_r$; (c) $-J_1 n_i n_{i+1} = J_1 a_i^{\dagger} a_{i+1}^{\dagger} a_{i+1} a_i$.

This calculation is hard to extend to ΔE_k for larger k using naive perturbation theory. We need a more powerful formalism, namely Matsubara diagrams. In this formalism one has diagrams constructed from the following elements. The perturbations V_1 , V_2 , and V_3 are represented by vertices as shown in Fig. 6. Each such vertex carries the appropriate factor $[(-h/2), -J_1\delta_{r,k}$, and $-J_1$, respectively, where $\delta_{r,k}$ is the Kronecker delta; also note that at leading order $J_{i,i+1} = J_1$, because we never invoke the term $J_{k,k+1}$. Lines labeled with the same index are joined and a sum is taken over all topologically inequivalent connected diagrams. Each line represents a Green's function $(z_v - \Delta)^{-1}$. All the indices are summed over. The z's are summed over the Matsubara frequencies $z_v = 2v\pi i/(k_B T)$, where v runs over all integers positive and negative. One enforces conservation of z, that is, for each vertex the sum of all incoming z's minus the sum of all outgoing z's must equal zero. For the present case, this conservation law mean that at any vertex which has only one line entering or leaving, the

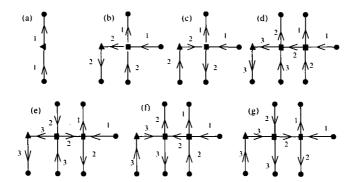


Fig. 7. Matsubara diagrams. The vertices are explained in the preceding figure. The lines are labeled by an index i to represent the Green's function $(z-d)^{-1}$. This calculation is for a linear system with sites labeled 1, 2,.... These diagram give $-\Delta E_m$ following the reasoning of Figs. 4 and 5. (a) For m=0; (b, c) for m=1; (d-g) for m=2. No new topology is obtained by reversing the direction of the line labeled 1. However, one may independently reverse the direction of all other lines giving rise to a degeneracy 2^m .

corresponding z must be zero. One can quickly see that the z's for all lines have to be zero. So, in fact, there is no sum over z to be done. (Such sums normally lead to the Bose occupation number factors.)

From Fig. 7 we see that

$$\Delta E_0 = -E_a \tag{3.15}$$

where E_a is the energy from diagram (a) of Fig. 7. (A similar notation for the other diagrams is used below.) Thus

$$\Delta E_0 = -(-h/2)(-J_1)(-h/2)(-\Delta)^{-2} = h^2 J_1/(4\Delta^2) = h^2 J_1/(16J_0^2) \quad (3.16)$$

as before. To obtain this result, note that diagram (a) has two filled circle vertices (each carrying a factor -h/2), one triangle (carrying a factor $-J_1$), and two lines, each of which carries a factor $(z-E_i)^{-1} = -\Delta^{-1}$. Also from Fig. 7 we have

$$\Delta E_1 = -(E_b + E_c) = -2E_b \tag{3.17}$$

Since diagram (b) has four h vertices, two J_1 vertices, and five lines, we have that

$$\Delta E_1 = -2(-h/2)^4 (-J_1)(-J_1)(-\Delta)^{-5} = h^4 J_1^2 / (8\Delta^5) = h^4 J_1^2 / (256J_0^5)$$
 (3.18)

Finally, from Fig. 7 we have

$$\Delta E_2 = -(E_d + E_e + E_f + E_g) = -4E_d \tag{3.19}$$

Since diagram (d) has six h vertices, three j vertices, and eight lines

$$\Delta E_2 = -4(-h/2)^6 (-J_1)(-J_1)^2 (-\Delta)^{-8} = h^6 J_1^3 / (16\Delta^8) = h^6 J_1^3 / (4096J_0^8)$$
(3.20)

Evidently, the general result is

$$\Delta E_k = J_0 (J_1 h^2 / 16 J_0^3)^{k+1} \tag{3.21}$$

4. CONCLUSIONS

Equation (3.21) indicates that the boundary between phases with k=p and k=p+1 is given to leading order by $H_p^*=-J_0(J_1h^2/16J_0^3)^{p+1}$. The resulting phase diagram is shown schematically in Fig. 8.

The analysis presented above was based on retaining only the leading-order (in h/J_0 and J_1/J_0) term in the surface-interface interaction. Although

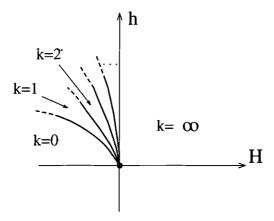


Fig. 8. Schematic representation of the phase diagram for interface unbinding transitions in the transverse Ising model.

we cannot rule out the possibility that the neglected higher order interactions could become dominant for very large k (for fixed h and J_0), we do not expect to observe any qualitative corrections to the phase diagram in this limit. This is because there are no competing interactions which would make correlation functions oscillatory at large distance and therefore it seems implausible that the positive sign of ΔE_p can be changed by the neglected higher order terms.⁽¹⁴⁾

To summarize, we have shown that quantum fluctuations can stabilize an infinite sequence of layering transitions in a three-dimensional transverse Ising model.

ACKNOWLEDGMENTS

We thank Malte Henkel for helpful discussions. Work at the University of Pennsylvania was partially supported by the National Science Foundation under grant 95-20175. J.M.Y. acknowledges support from the EPSRC, and C.M. from the EPSRC and the Fondazione "A. della Riccia," Florence.

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